

Results from $n^3\text{He}$ Target Chamber Voltage Scan

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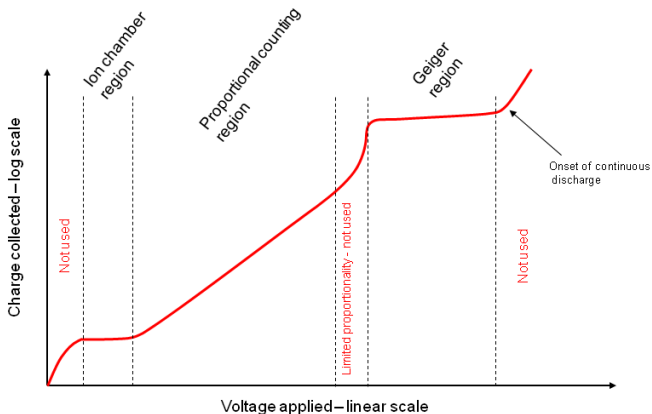
March 14, 2016

- ① Introduction
- ② Fitting Parameters
- ③ 1V Ripple
- ④ Asymmetries
- ⑤ Target Stability With Beam Power Changes
- ⑥ Inversion Scan

Basic Modes of Operation

Practical Gaseous Ionisation Detector Regions

Variation of ion pair charge with applied voltage in a wire cylinder system with constant incident radiation.



Fitting Method

For fitting the proportional region first a constant line from 200 - 340V was fit in the ionization region for most wires. This was used to set p_0 in the piece wise function

$$f(x) = \begin{cases} p_0 & \text{if } x < p_2 \\ p_0 + p_1(x - p_2)^2 & \text{if } x > p_2 \end{cases} \quad (1)$$

Root Formula Definition:

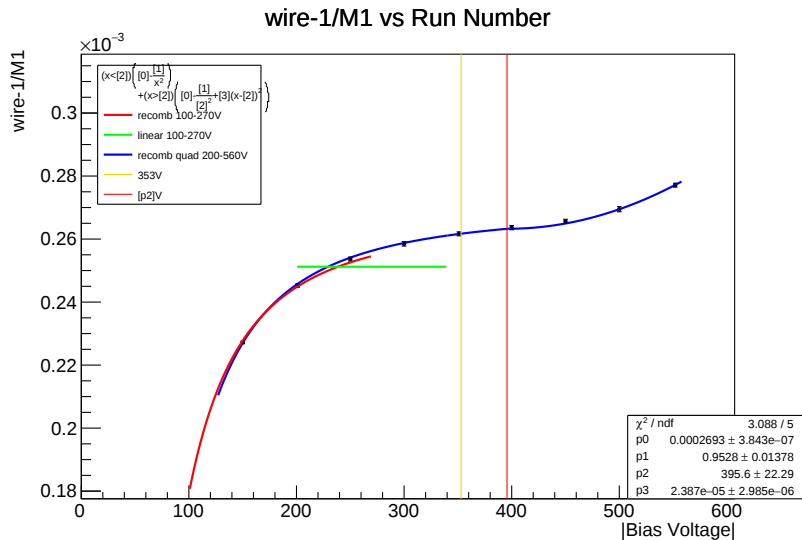
```
TF1 *fm3 = new TF1("fm3", "(x<[2])*[0] + (x>[2])*([0]+([1]*(x-[2]))**2)", 200, 560);
```

giving a continuous curve that starts linear and transitions at voltage p_2 to quadratic. Outer wires from 1-70 where ion chamber region was very small or nonexistent were fit as:

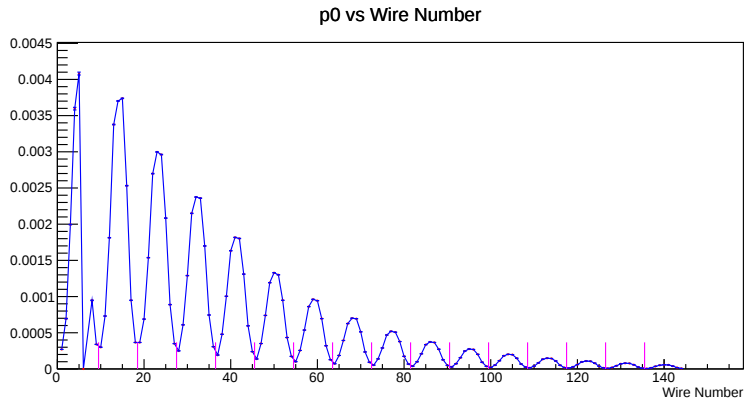
$$f(x) = \begin{cases} p_0 - p_1/x^2 & \text{if } x < p_2 \\ (p_0 - p_1/p_2^2 + p_3(x - p_2)^2 & \text{if } x > p_2 \end{cases} \quad (2)$$

```
TF1 *fm3 = new TF1("fm3", "(x<[2])*([0]-[1]/x**2) + (x>[2])*([0]-[1]/p2**2 + ([3]*(x-[2]))**2)", 100, 560);
```

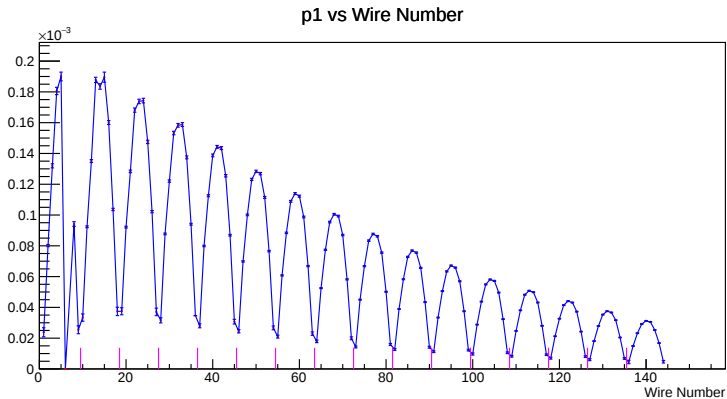
Outer Wire Fitting Example



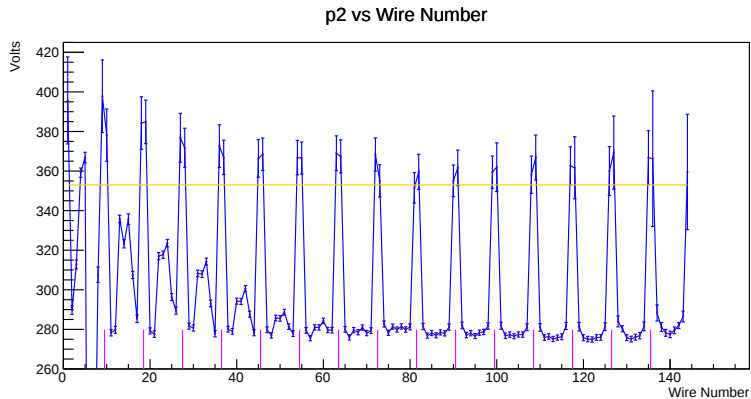
p0 vs Wire Number



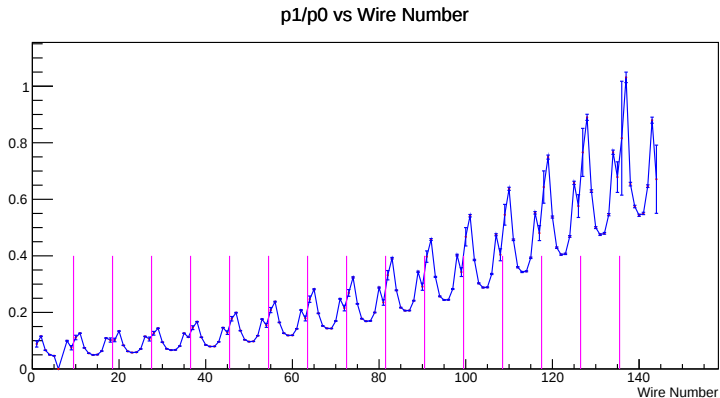
p1 vs Wire Number



p2 vs Wire Number

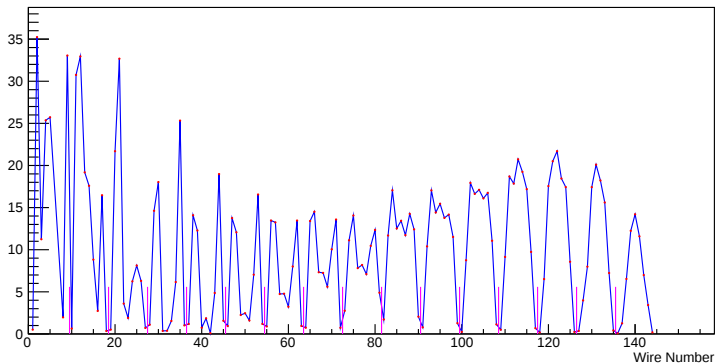


$p1/p0$ vs Wire Number

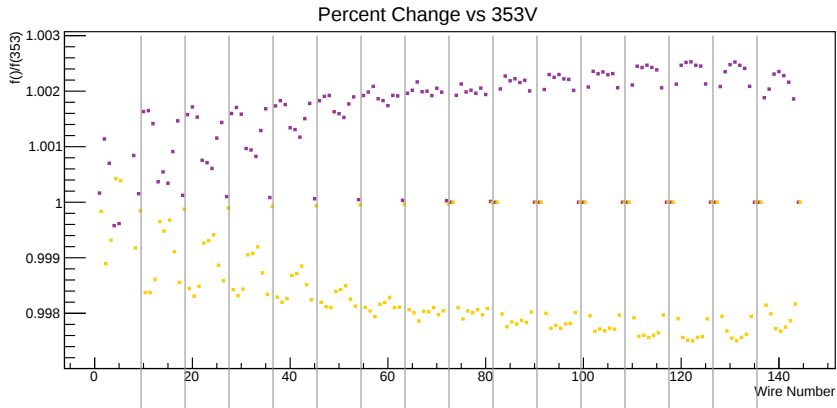


χ^2/NDF vs Wire Number

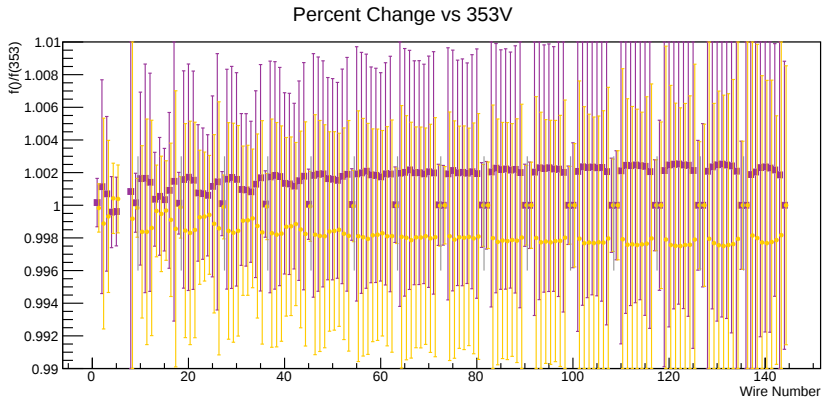
Chi Squared/NDF vs Wire Number



Effect of 1V Ripple - without error bars



Effect of 1V Ripple - with error bars



Depending which wire ionization occurs around it will have a different rate of ionization collection with most wires collecting slightly more ionization than occurred around the wire. This gives an effective increase in the gain that changes across the chamber.

$$A_1 = \frac{g_{amp}g_{gas}I^{\uparrow} - g_{amp}g_{gas}I^{\downarrow}}{g_{amp}g_{gas}I^{\uparrow} + g_{amp}g_{gas}I^{\downarrow}} \quad (3)$$

$$= \frac{g_{amp}g_{gas}}{g_{amp}g_{gas}} \frac{I^{\uparrow} - I^{\downarrow}}{I^{\uparrow} + I^{\downarrow}} \quad (4)$$

$$= \frac{I^{\uparrow} - I^{\downarrow}}{I^{\uparrow} + I^{\downarrow}} \quad (5)$$

Two Wire Geometric Asymmetry

$$R_{ij}^{\uparrow/\downarrow} = \frac{g_{amp,i} g_{gas,i} l_i^{\uparrow/\downarrow}}{g_{amp,j} g_{gas,j} l_j^{\uparrow/\downarrow}} \quad (6)$$

$$A_2 = \frac{R_{ij}^{\uparrow} - R_{ij}^{\downarrow}}{R_{ij}^{\uparrow} + R_{ij}^{\downarrow}} \quad (7)$$

$$= \frac{\frac{g_{amp,i} g_{gas,i} l_i^{\uparrow}}{g_{amp,j} g_{gas,j} l_j^{\uparrow}} - \frac{g_{amp,i} g_{gas,i} l_i^{\downarrow}}{g_{amp,j} g_{gas,j} l_j^{\downarrow}}}{\frac{g_{amp,i} g_{gas,i} l_i^{\uparrow}}{g_{amp,j} g_{gas,j} l_j^{\uparrow}} + \frac{g_{amp,i} g_{gas,i} l_i^{\downarrow}}{g_{amp,j} g_{gas,j} l_j^{\downarrow}}} \quad (8)$$

$$= \frac{\frac{g_{amp,i} g_{gas,i}}{g_{amp,j} g_{gas,j}} \frac{l_i^{\uparrow}}{l_j^{\uparrow}} - \frac{l_i^{\downarrow}}{l_j^{\downarrow}}}{\frac{g_{amp,i} g_{gas,i}}{g_{amp,j} g_{gas,j}} \frac{l_i^{\uparrow}}{l_j^{\uparrow}} + \frac{l_i^{\downarrow}}{l_j^{\downarrow}}} = \frac{\frac{l_i^{\uparrow}}{l_j^{\uparrow}} - \frac{l_i^{\downarrow}}{l_j^{\downarrow}}}{\frac{l_i^{\uparrow}}{l_j^{\uparrow}} + \frac{l_i^{\downarrow}}{l_j^{\downarrow}}} \quad (9)$$

Asymmetries from Elise's Presentation

Two detector asymmetry from NDGamma

$$A_{exp} = \frac{(\sum S_{up} - \sum S_{dn})_{d1} - (\sum S_{up} - \sum S_{dn})_{d2}}{(\sum S_{up} + \sum S_{dn})_{d1} + (\sum S_{up} + \sum S_{dn})_{d2}} \quad (10)$$

Beam Asymmetry

$$A_B = \frac{(\sum S_{up} - \sum S_{dn})_{d1} + (\sum S_{up} - \sum S_{dn})_{d2}}{(\sum S_{up} + \sum S_{dn})_{d1} + (\sum S_{up} + \sum S_{dn})_{d2}} \quad (11)$$

Detector Asymmetry

$$A_D = \frac{(\sum S_{up} + \sum S_{dn})_{d1} - (\sum S_{up} + \sum S_{dn})_{d2}}{(\sum S_{up} + \sum S_{dn})_{d1} + (\sum S_{up} + \sum S_{dn})_{d2}} \quad (12)$$

$$\alpha = \left[\frac{N_i^\uparrow}{N_i^\downarrow} \right] \left[\frac{N_{i+6}^\uparrow}{N_{i+6}^\downarrow} \right] \quad (13)$$

$$A_i^{raw} = \frac{\sqrt{\alpha} - 1}{\sqrt{\alpha} + 1} \quad (14)$$

Beam Power Scan

- Very rarely was beam power changed significantly during a run where we took data.
- Instead use runs over full duration of data taking to sample different powers
- 16 runs chosen
- M1 Integral ran from $4e6$ to $7.5e6$
- nearly 100% beam power change

List of Runs

19484(shutter closed)

18014

22014

26014

29914

34014

38024

41914

46014

48012

48014

48015

50014

52014

54014

57014

- Integrated each pulse in a run for all wires and M1

$$x_{j,i} = \frac{1}{60 \times N} \sum_{k=1}^N s_{j,i}(k) \quad N = 49 \text{ or } 1624 \quad (15)$$

where $x_{j,i}$ is the integrated total of the i th pulse in the j th run.

- Average pulse integrals and form standard error for run averages

$$Avg = \langle x_j \rangle = \frac{1}{q} \sum_{i=1}^q x_{j,i} \quad (16)$$

q = number of uncut entries in run

$$StdErr = \frac{\sigma}{\sqrt{q}} = \frac{1}{\sqrt{q}} \sqrt{\langle x^2 \rangle - \langle x \rangle^2} \quad (17)$$

- M1 cut used to remove dropped pulses if $M1[600] < 0.9 \langle M1[600] \rangle$
- M1 and Chamber correlations not accounted for.

Method

A beam off power supply off run was used as the pedestal and designated by $j = 0$. The wire and M1 values were pedestal subtracted before division.

$$R_j = \frac{\langle x_j \rangle - \langle x_0 \rangle}{\langle M1_j \rangle - \langle M1_0 \rangle} \quad (18)$$

Error Propagation:

$$C = A - B \quad (19)$$

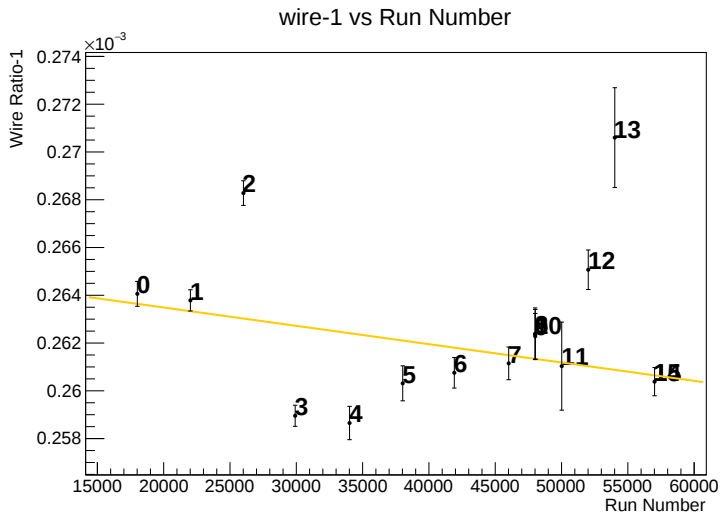
$$\sigma_C = \sqrt{\sigma_A^2 + \sigma_B^2} \quad (20)$$

$$C = \frac{A}{B} \quad (21)$$

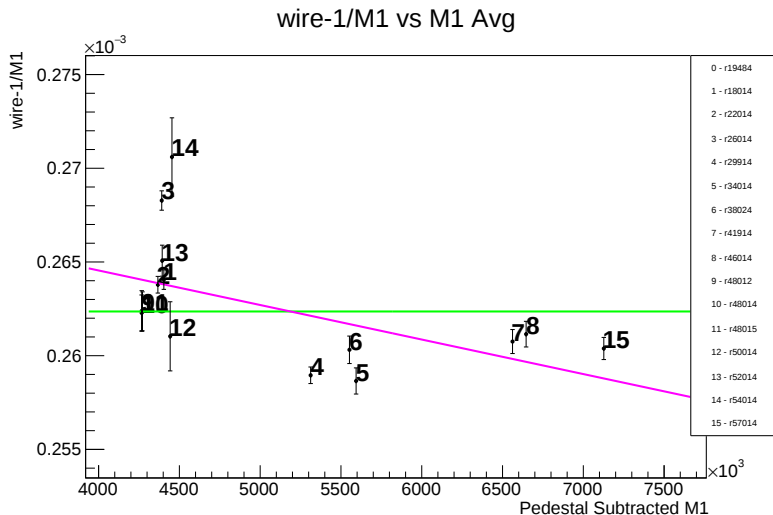
$$\sigma_C = \frac{A}{B} \sqrt{\left(\frac{\sigma_A}{A}\right)^2 + \left(\frac{\sigma_B}{B}\right)^2} \quad (22)$$

where σ is the uncertainty for the values.

Wire 1 / M1 vs. Run Number

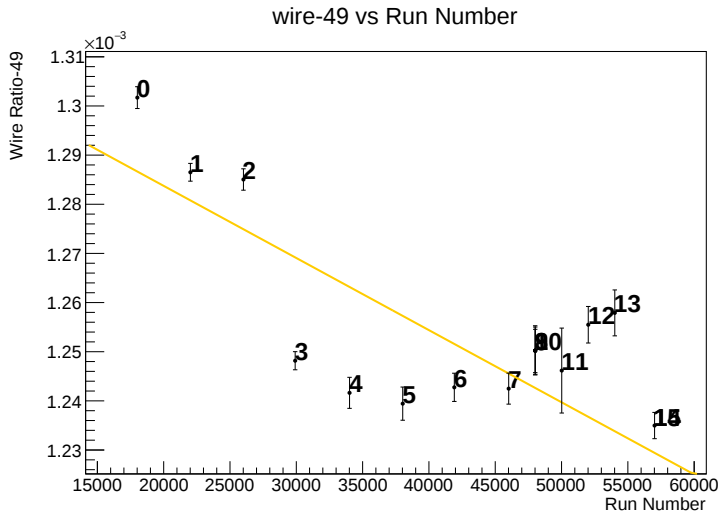


Wire 1 / M1 vs. M1



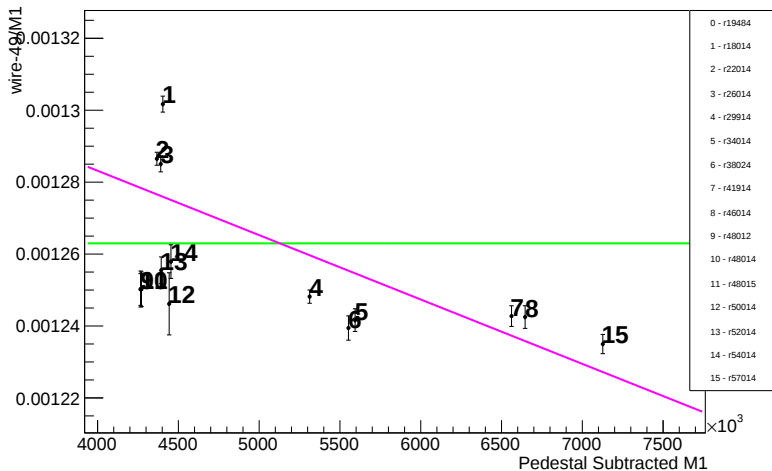
- [0] fit line (green line)
- [0] + [1] * x (magenta line)
- both around χ^2/NDF from 10-14

Wire 49 / M1 vs. Run Number

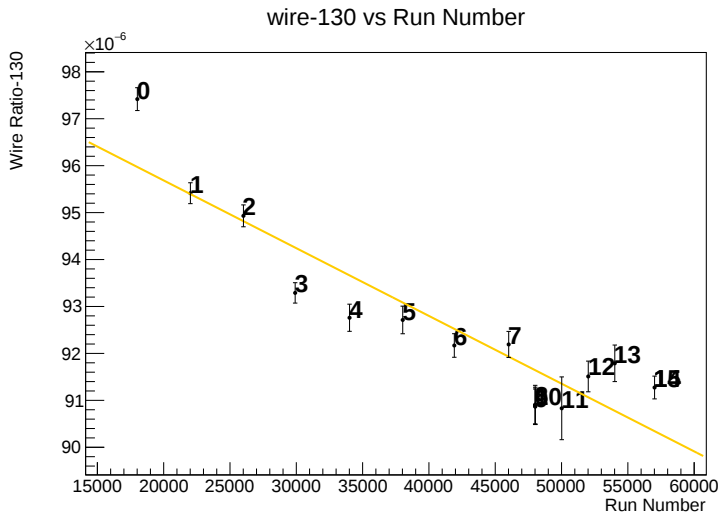


Wire 49 / M1 vs. M1

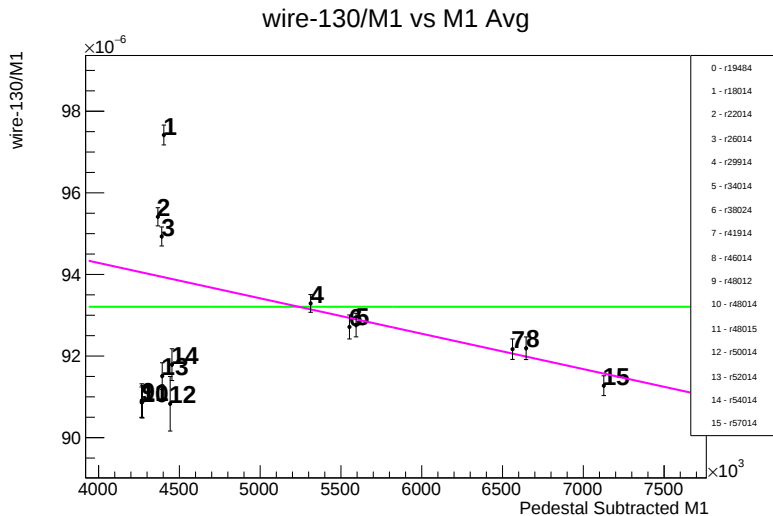
wire-49/M1 vs M1 Avg



Wire 130 / M1 vs. Run Number



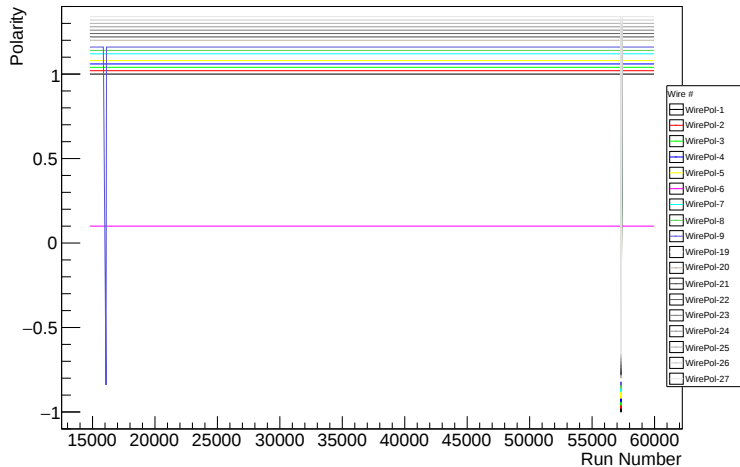
Wire 130 / M1 vs. M1



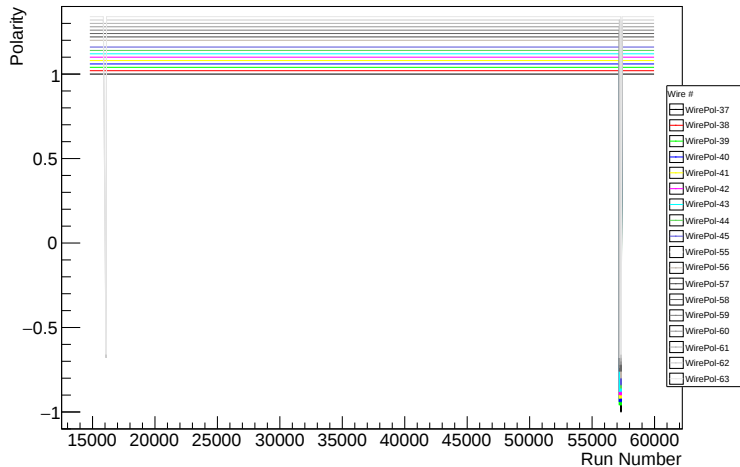
Wire Inversion Scan Method

- Used the condensed data set
- the sign of each wire was found by summing every 103rd pulse in each run, and checking if the sum was greater or less than zero.
- each wire in each run assigned value +1 or -1
- wire 6 assigned value 0 in all runs

Daq21A

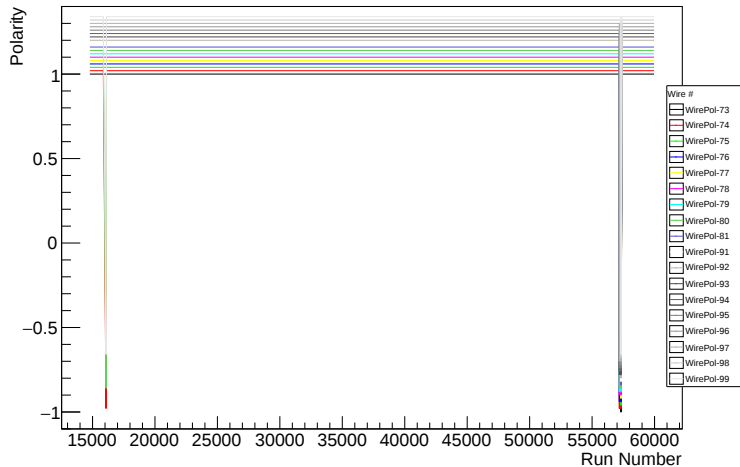


Daq21B

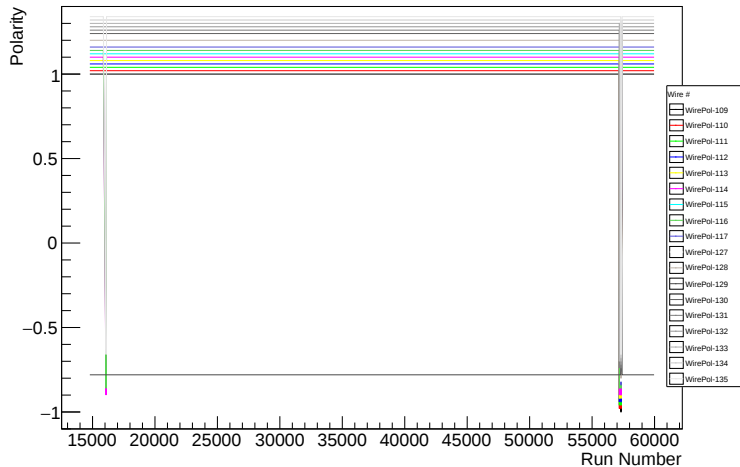


Daq2- channels 0-17

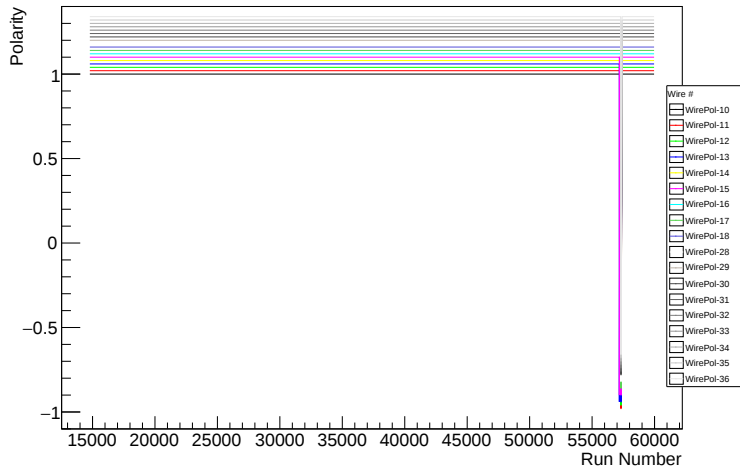
Daq22A



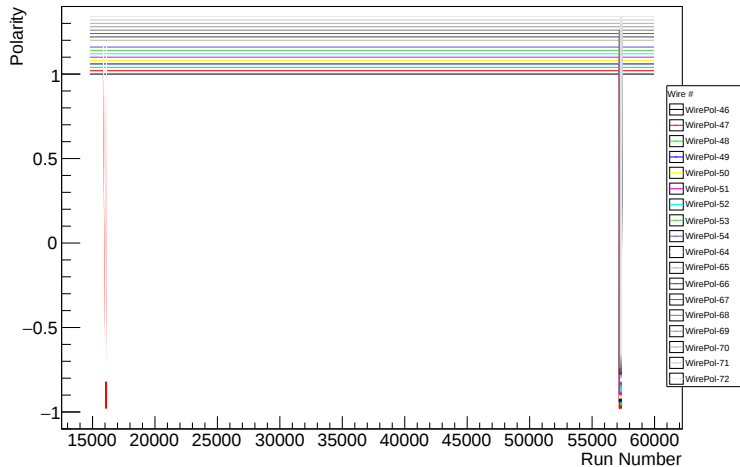
Daq22B



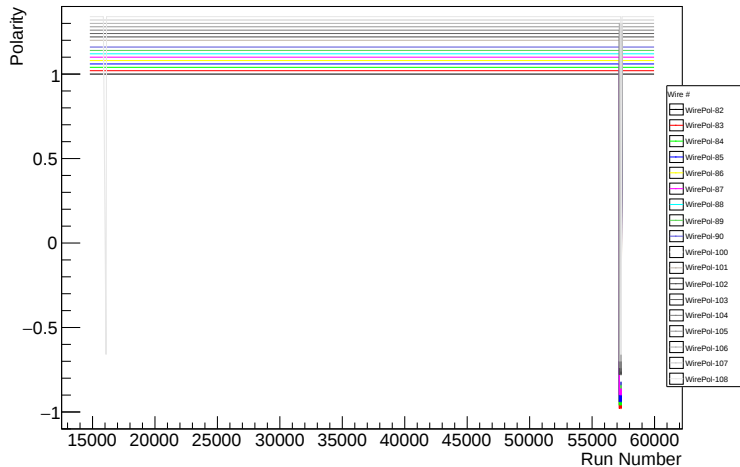
Daq23A



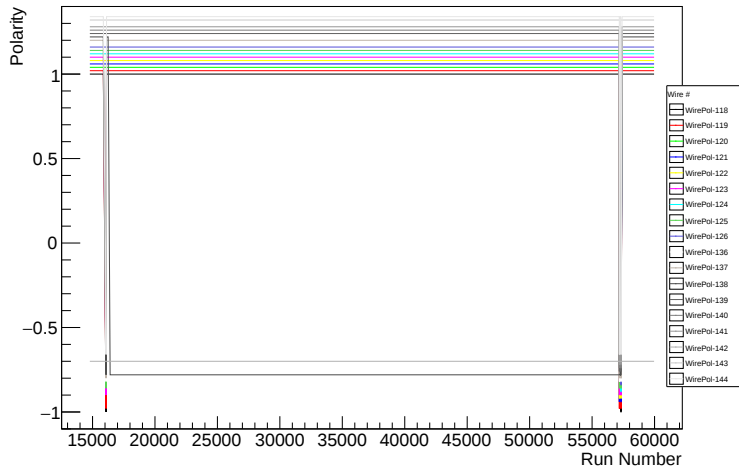
Daq23B



Daq24A



Daq24B



Inversion Locations

- run 16082 inverted
 - inverted wires: 9, 47, 62, 63, 64, 74, 80, 99, 100, 108, 114, 116, 118, 119, 123, 135, 136, 137, 138, 144
- run 16121 above reverted
- changed at run 16410 wire 138 + to -
- changed at run 57255 wire 138 - to +
- changed at run 57266 wire 138 + to -
- changed at run 57277 wire 138 - to +
- changed at run 57283 wire 138 + to -
- 57314 most wires inverted until 57403
 - wire not changed: 10, 16, 18, 29, 38, 46, 55, 59, 82, 88, 105, 107, 120, 142, 143

Inversion within a run not thoroughly checked. No indications of mid run changes from other work.